

AL1666A

### HIGH PERFORMANCE DIMMABLE LED CONTROLLER

## Description

The DIODES<sup>™</sup> AL1666A is a high performance single stage Flyback and Buck-boost controller, targeting dimmable LED lighting application. It is a primary side regulation (PSR) controller which can provide accurate Constant Current (CC) regulation without optocoupler and secondary control circuitry. It is operating at BCM mode which results in good EMI and efficiency, and keeps high PF and low THD under universal input voltage.

The AL1666A can support analog/PWM dimming modes. When a 0 to 2.4V DC signal is applied on ADIM pin, the device will operate in analog dimming mode; when a digital signal is applied on PWMD pin and the ADIM pin is connected with hundreds of nF capacitors, the device will work at PWM-to-DC dimming mode. The dimming range is 1% to 100%.

The AL1666A has rich protection features. It integrates multiple protections including Under Voltage Lock Out (UVLO), Output Over Voltage Protection (OVP), Output Short Circuit Protection (OSP), Over Current Protection (OCP), Winding Short Circuit, Secondary Diode Short, Internal Thermal Fold-Back Protection (TFP) and Over Temperature Protection (OTP).

The AL1666A is available in SO-8 (Standard) package.

## Features

- Primary Side Regulation without Opto-Coupler
- Valley Switching for Low Switching Loss
- Support Analog and PWM-to-DC Dimming
- Analog/PWM-to-DC Dimming Range: 1 to 100%
- Tight CS Reference Voltage 0.4V±1.5%
- High PF > 0.9 and Low THD < 20%
- High Efficiency
- Internal Protections
  - Under Voltage Lock Out (UVLO)
  - Output Over Voltage Protection (OVP)
  - Output Short Protection (OSP)
  - Over Current Protection (OCP)
  - Winding Short Circuit Protection
  - Secondary Diode Short Protection
  - Internal Thermal Fold-back Protection (TFP)
  - Over Temperature Protection (OTP)
- Tight LED Current Variation Range LED Current Line Regulation: ±2% (90V<sub>AC</sub> to 305V<sub>AC</sub>) LED Current Load Regulation: ±2% Full Load to Half Load
- Package: SO-8 (Standard)
- Totally Lead-Free & Fully RoHS Compliant (Notes 1 & 2)
- Halogen and Antimony Free. "Green" Device (Note 3)
- For automotive applications requiring specific change control (i.e. parts qualified to AEC-Q100/101/104/200, PPAP capable, and manufactured in IATF 16949 certified facilities), please <u>contact us</u> or your local Diodes representative. <u>https://www.diodes.com/quality/product-definitions/</u>

Notes: 1. No purposely added lead. Fully EU Directive 2002/95/EC (RoHS), 2011/65/EU (RoHS 2) & 2015/863/EU (RoHS 3) compliant.

- 2. See https://www.diodes.com/quality/lead-free/ for more information about Diodes Incorporated's definitions of Halogen- and Antimony-free, "Green" and Lead-free.
- 3. Halogen- and Antimony-free "Green" products are defined as those which contain <900ppm bromine, <900ppm chlorine (<1500ppm total Br + Cl) and <1000ppm antimony compounds.

### Pin Assignments



SO-8 (Standard)

### Applications

- General LED lighting drivers with dimming functions
- OV to 10V dimming luminaires
- General purpose constant current sources
- Smart LED lightings



# **Typical Applications Circuit**



Figure 1 Flyback Application Circuit





Figure 3 AL1666A Combined with DIODES<sup>™</sup> AL8116 & DIODES<sup>™</sup> AL5822 to Achieve 0-10V Dimming



# **Pin Descriptions**

Pin Number	Pin Name	Function		
1	ADIM	Analog Dimming Input Pin		
2	PWMD	PWM Signal Input Pin		
3	COMP	Loop Compensation Pin		
4	CS	Current Sense Pin, Connect This Pin to The Source of The Primary Switch		
5	GND	Ground		
6	OUT	Gate Driver Output		
7	VCC	Supply Voltage of Gate Driver and Control Circuits of The IC		
8	FB	The Feedback Voltage Sensing from the Auxiliary Winding		

# Functional Block Diagram



Figure 4 AL1666A Block Diagram



## **Absolute Maximum Ratings** (@T<sub>A</sub> = +25°C, unless otherwise specified.) (Note 4)

Symbol	Parameter	Rating	Unit
Vcc	Power Supply Voltage	-0.3 to 30	V
Vcs	Voltage at CS to GND	-0.3 to 7	V
V <sub>FB</sub>	FB Input	-0.3 to 7	V
VCOMP	Loop Compensation Pin	-0.3 to 7	V
Vout	Driver Output Voltage	-0.3 to 20	V
VPWMD	Voltage at PWMD to GND	-0.3 to 7	V
VADIM	Voltage at ADIM to GND	-0.3 to 7	V
TJ	Operating Junction Temperature	-40 to +150	°C
T <sub>STG</sub>	Storage Temperature	-65 to +150	°C
TLEAD	Lead Temperature (Soldering, 10s)	+300	°C
PD	Power Dissipation at T <sub>A</sub> = +50°C	0.65	W
θ <sub>JA</sub>	Thermal Resistance (Junction to Ambient)	136	°C/W
θις	Thermal Resistance (Junction to Case)	30	°C/W
	ESD (Human Body Model)	2000	V
—	CDM (Charged-Device Model)	1000	V

Note: 4. Stresses greater than those listed under Absolute Maximum Ratings can cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions is not implied. Exposure to Absolute Maximum Ratings for extended periods can affect device reliability. All voltages unless otherwise stated and measured with respect to GND.

# Recommended Operating Conditions (@TA = +25°C, unless otherwise specified.)

Symbol	Parameter	Min	Мах	Unit
TA	Ambient Temperature (Note 5)	-40	+105	°C
Vcc	Operating VCC Voltage (Note 6)	8.5	23	V

Notes: 5. The device may operate normally at +125°C ambient temperature under the condition not triggers temperature protection. 6. I<sub>CC</sub> should be limited less than 5mA.



## Electrical Characteristics (@T<sub>A</sub> = +25°C, unless otherwise specified.)

Symbol	Parameter	Conditions	Min	Тур	Мах	Unit
JVLO Section	•	. I		•		
Vcc_тн	Startup Threshold Voltage	_	13.4	15	16.5	V
VOPR_MIN	Minimal Operating Voltage	After Turn On	5.8	7.8	9	V
standby Current S	Section			1		
Ist	Startup Current	Vcc = Vcc_TH -0.5V, before Start Up		120	300	μA
lcc	Operating Current @4kHz	$\label{eq:VCC} \begin{array}{l} V_{CC} = 20V, \ V_{DIM} = 3V, \ V_{FB} = V_{CS} = \\ V_{COMP} = 1V, \ C_{OUT} = 1nF \end{array}$	_	2	4	mA
Prive Output Section	ion					
tR	Output Voltage Rise Time (Note 7)	C <sub>L</sub> = 1nF		100	—	ns
tF	Output Voltage Fall Time (Note 7)	C <sub>L</sub> = 1nF	_	100	_	ns
Vout_clamp	Output Clamp Voltage	Vcc = 20V	9.8	12	15.5	V
ton_min	Minimum On Time (Note 7)	—	_	1000	2010	ns
ton_max	Maximum On Time	_		15	_	μs
toff_max	Maximum Off Time	_	_	290	405	μs
fmax	Maximum Frequency	—		150	_	kHz
nternal CS Refere	nce					
		T <sub>A</sub> = +25°C	0.394	0.4	0.406	V
VREF	Internal Reference Voltage	$T_{A} = -40^{\circ}C \text{ to } +105^{\circ}C$	0.392	0.4	0.415	V
Vcs_clamp	Primary Current Clamp Voltage	_	_	2	_	V
Vcs_ocp	Primary Over Current Voltage	_	_	3	_	V
Fror Amplifier				1		
Gm	Trans-Conductance	_	_	27	_	μA/\
ISOURCE	Amplifier Source Current	_	_	7.2	_	μA
eedback Input Se	ection					
V <sub>FB_CV</sub>	FB CV Threshold	_	2.86	3.0	3.26	V
WMD Section		-				
Vpwm_l	PWM Signal Low Threshold Voltage	_	_	_	0.4	V
V <sub>PWM_H</sub>	PWM Signal High Threshold Voltage	_	2.0	_		V
fpwm	PWM Frequency for PWM to DC Dimming	—	0.5	_	20	kHz
DIM Section						•
_	Analog Dimming Range on ADIM	_	0.05	_	2.4	V
_	Analog Dimming High Level	_	2.35	2.4	2.45	V
_	Analog Dimming Range Ratio	_	1	_	100	%
hermal Fold-Bac	k Section	1		1	L	1
T <sub>REG</sub>	Overheating Temperature Regulation (Note 7)	_	_	+150	_	°C
Over Temperature	Protection Section			1		I
	Shutdown Temperature (Notes 7, 8)	1 1		+180		°C

8. At startup, when V<sub>CC</sub> reaches V<sub>CC\_TH</sub>, the controller blanks OTP for more than 250µs to avoid detecting an OTP fault by allowing the PWMD pin voltage to reach its nominal value if a filtering capacitor is connected to the PWMD pin.



### Performance Characteristics (Note 9)

### Startup Threshold Voltage vs. Ambient Temperature



### CS Reference Voltage vs. Ambient Temperature



**Operating Current vs. Ambient Temperature** 





Minimum Operating Voltage vs. Ambient Temperature



Startup Current vs. Ambient Temperature





## Performance Characteristics (continued)

### CS Clamp Reference Voltage vs. Ambient Temperature



FB CV Threshold vs. V<sub>CC</sub> Voltage



**Analog Dimming Curve** 



FB CV Threshold vs. Ambient Temperature



CS Reference Voltage vs. V<sub>CC</sub> Voltage



Analog Dimming Curve (Zoomed in 0 to 10%)





## **Application Information**

The AL1666A is a constant current high PF Flyback and Buck-boost controller with Primary Side Regulation (PSR), targeting LED lighting applications. The device eliminates the opto-couplers or the secondary feedback circuits, which will help to minimize the whole system BOM cost. High power factor is achieved by constant on-time operation. In order to reduce the switching losses and improve EMI performance, quasi-resonant switching mode is applied. The AL1666A integrates multiple protections including UVLO protection, output open voltage protection, over current protection, thermal fold-back protection and over temperature protection. The AL1666A can support analog dimming mode and PWM dimming.

#### Start-Up

After AC supply is powered on, the capacitor  $C_{VCC}$  across VCC pin and GND pin will be charged up by BUS voltage through a start-up resistor R<sub>TH</sub>. Once V<sub>CC</sub> reaches V<sub>CC\_TH</sub>, the internal blocks start to work. V<sub>CC</sub> is supplied by V<sub>BUS</sub> until the auxiliary winding of Flyback transformer could supply enough energy to maintain V<sub>CC</sub> above V<sub>OPR\_MIN</sub>. If V<sub>CC</sub> voltage is lower than V<sub>OPR\_MIN</sub>, the switch will be turned off.

After Vcc exceeds Vcc\_TH, the drive blocks don't start to switch on/off signals until VcomP is higher than the initial voltage VcomP\_sT which can be programmed by RcomP. The formula is shown as below. Such design can program startup on time to reduce the startup time or reduce the output overshoot current.

$$V_{COMP \_ST} = 1.4V - 700 \ \mu A \cdot R_{COMP}$$

Where VCOMP\_ST is the pre-charged voltage of COMP pin, RCOMP is shown as Figure 1.

Generally, a big capacitance of C<sub>COMP</sub> is necessary to achieve high power factor and stabilize the system loop (1µF to 2µF is recommended). The pre-charged voltage in start-up procedure can be programmed by R<sub>COMP</sub>.

#### Protections

#### 1. Output Open Protection (OVP)

The output voltage is reflected by the voltage on transformer's auxiliary winding. FB pin of IC integrates over voltage protection function. When there is a rapid line and load transient, the output voltage may exceed the regulated value. If VFB exceeds VFB\_CV, the FB over voltage protection will be triggered, switch will be turned off and the IC will discharge VCC. When the VCC is below the VOPR\_MIN voltage, IC will restart and the VCC capacitor is charged again by start-up resistor. If the over voltage condition still exists, the system will work in hiccup mode.

Thus, output over voltage depends on the minimum voltage between both OVP protections' limitation. It can be gotten by below formula.

$$V_{OVP} = \frac{N_S}{N_{AUX}} \cdot \frac{R5 + R6}{R6} \cdot V_{FB\_CV}$$

Where: R5 and R6, shown as Figure 1, divide reflected voltage.

 $N_{\text{AUX}}$  is the turns of auxiliary winding.

N<sub>S</sub> is turns of the secondary winding.

#### 2. Output Short Protection (OSP)

When the output is shorted, the output voltage is clamped to zero. The output voltage of the auxiliary winding, which is proportional to the output winding, will drop down too. If  $V_{FB}$  drops below 0.4V, the output short protection will be triggered, the device cannot detect the toFF time, and the device controls the system operation at 4kHz low frequency.

#### 3. Over Current Protection (OCP)

The AL1666A has a built-in cycle by cycle over current protection of primary inductor current. When CS pin voltage reaches the voltage V<sub>CS\_CLAMP</sub>, switch will be turned off until next switch period. The maximum peak current (I<sub>PEAK (MAX)</sub>) of the inductor can be calculated as below:

$$I_{PEAK\_MAX} = \frac{V_{CS\_CLAMP}}{R_{CS}}$$

Where:

 $V_{CS\_CLAMP}$  means primary current clamp voltage that is 2V.  $R_{CS}$  is current sense resistor shown in Figure 1.



#### 4. Secondary Diode/Primary Windings/Secondary Windings Short Protection

The CS voltage will be high when Secondary Diodes/Primary windings/Secondary windings are shorted. If CS is higher than  $V_{CS\_OCP}$ , the protection will be triggered, switch will be turned off and  $V_{CC}$  will be latched for 1s, then  $V_{CC}$  will be discharged. Once  $V_{CC}$  is below  $V_{OPR\_MIN}$ , the IC will shut down and power on again by the BUS voltage through the startup resistor. Power dissipation is low when output short protection happens.

#### 5. Thermal Fold-Back Protection (TFP)

The AL1666A has thermal fold-back function: it adopts self-adaptive control method which can prevent the system from breaking down caused by over temperature. The overheating temperature is set at +150°C. When the temperature of the IC is higher than this point, the device will decrease the voltage reference of the CS linearly until OTP happens. By this way, the device can limit system's input power at high ambient temperature, preventing system's temperature increases further.

#### 6. Over Temperature Protection (OTP)

The AL1666A has built-in Over Temperature Protection (OTP) function. When the temperature goes up to +180°C, the over temperature protection is triggered, which leads to VCC UVLO. When OTP recovers, the system can be restarted.

#### **Application Note:**

#### **Output Constant-current Control**

According to the definition of mean output current, the mean output current can be obtained as below.

$$I_{O_{-MEAN}} = \frac{1}{\pi} \cdot \int_{0}^{\pi} \frac{1}{2} \cdot I_{SP} \cdot \frac{t_{ONS}}{t_{SW}} dt$$

Where  $I_{O\_MEAN}$  is the mean output current; Isp is secondary peak current of transformer;

 $\ensuremath{\mathsf{tons}}$  is discharge time of secondary side of transformer;  $\ensuremath{\mathsf{tsw}}$  is the switch period.

According to the principle of AL1666A close loop control, the voltage of Rcs will be sampled when switch is turned off and the value will be held until discharge time tons is over. It can be described by following formula:

$$V_{REF} = \frac{l}{\pi} \int_{0}^{\pi} I_P \cdot R_{CS} \cdot \frac{t_{ONS}}{t_{SW}} dt$$

Where IP is primary peak current of transformer; Rcs is current sense resister which is shown as Figure 1.

tons is discharge time of secondary side of transformer; tsw is the switch period. VREF is internal reference voltage that is equal to 0.4V.

The peak current at secondary side has following relationship with primary side peak current, if the effect of the leakage inductor is neglected.

$$I_{SP} = N_{PS} \cdot I_P$$

Where NPs is the turns ratio of Flyback transformer (NPs=1 for Buck-boost); IP is the primary peak current of the transformer.

According to these above formulas, the mean output current can be induced finally by below expressions.

$$I_{O\_MEAN} = \frac{N_{PS} \cdot V_{REF}}{2 \cdot R_{CS}}$$

Where Io\_MEAN is the mean output current; Rcs is current sense resister which is shown as Figure 1 and Figure 2;

V<sub>REF</sub> is internal reference voltage that is equal to 0.4V; N<sub>PS</sub> is the turns ratio of Flyback transformer (N<sub>PS</sub> = 1 for Buck-boost); Therefore, the constant output current control can be realized with appropriate parameter design.



#### PF and THD Compensation Circuit

In typical application, the AL1666A can provide PF>0.9 and THD <20%. It can improve PF>0.95 and THD<10% by adding the below compensation circuit. V<sub>BUS</sub> is connected to bus line which is after rectifier bridge. COMP pin voltage will add an offset that almost follows with bus line voltage in the circuit. Due to COMP voltage controls switch-on time, thus phase difference between input voltage and input current will be reduced that can optimize PF and THD. In the circuit, range of resister value R12 is from 800k $\Omega$  to 1.5M $\Omega$ , range of resistor value R13 is from 500 $\Omega$  resistor to 5.1k $\Omega$ . Range of capacitance C11 is 1µF to 2µF. PF and THD can be improved by fine tuning these components.



Figure 5 PF and THD Optimization Circuit

#### Line Regulation Compensation Function

The AL1666A can achieve good line regulation by adjusting the FB pull-up resistor  $R_{FB1}$  and the CS external horizontal resistor  $R_{CS1}$ .  $R_{FB2}$  is the FB pull-down resistor. Figure 6 shows this circuit. As  $R_{FB2}$  is far larger than  $R_{FB3}$ , during  $t_{ONP}$ , the  $V_{FB}$  can be calculated approximately as:

$$V_{FB} = \frac{\sqrt{2} \cdot V_{IN\_RMS} \cdot N_{AP} \cdot R_{FB3}}{R_{FB1} + R_{FB3}}$$

And the Vcs\_offset can be got:

$$V_{CS\_OFFSET} = \frac{K \cdot \sqrt{2} \cdot V_{IN\_RMS} \cdot N_{AP} \cdot R_{FB3}}{R_{FB1} + R_{FB3}} \cdot (R_{CS1} + R_{CS2})$$

Where:

- K is conversion coefficient of I<sub>FB3</sub> that is equal to 0.013\*10<sup>-3.</sup>
- V<sub>IN\_RMS</sub> is the input RMS voltage.
- NAP is the turns' ratio of auxiliary winding and primary winding.
- R<sub>FB3</sub> is the internal FB pulldown resistor that is connected to the system during t<sub>ONP</sub> time and equals to 184Ω.
- R<sub>CS2</sub> is the internal horizontal resistor that is 6kΩ.

The output current can be calculated as:

$$I_{O\_MEAN} = \frac{N_{PS}}{2 \cdot R_{CS}} \cdot (V_{REF} - V_{CS\_OFFSET}) = \frac{N_{PS}}{2 \cdot R_{CS}} \cdot \left[ V_{REF} - \frac{K \cdot \sqrt{2} \cdot V_{IN\_RMS} \cdot N_{AP} \cdot R_{FB3}}{R_{FBI} + R_{FB3}} \cdot (R_{CSI} + R_{CS2}) \right]$$

Where:

• VREF is the internal reference voltage that is equal to 0.4V.



Figure 6 Line Regulation Compensation Circuit



#### **Dimming Mode**

The AL1666A can support two dimming modes: analog dimming and PWM-to-DC dimming.

#### 1. Analog Dimming Mode

In analog dimming mode, the dimming signal is added to ADIM pin directly to realize dimming function. The setting circuit is shown as Figure 7. When VADIM is higher than 2.4V, the driver will output 100% of rated current; when the voltage VADIM is in the range from 0mv to 2.4V, the output current will change linearly with the voltage VADIM. The dimming curve is shown as Figure 8 and the dimming range is from 1 to 100%.



Figure 7 Analog Dimming Setting Circuit

#### 2. PWM-to-DC Dimming Mode

In PWM-to-DC dimming mode, PWM dimming signal is added to PWMD pin. The setting circuit is shown as below. A capacitance of hundreds nF is recommended for CADIM. The duty cycle of the dimming signal DDIM is reflected by the voltage on ADIM pin VADIM.

 $V_{ADIM} = D_{DIM} \times 2.4V$ 

Where DDIM is duty of PWM signal; VADIM is the voltage of ADIM pin.



Figure 10 PWM Dimming Curve (PWM Frequency is 1kHz)

#### 3. 0-10V Dimming

Combined with general dimming controller AL8116, the AL1666A system also can operate with a 0-10V dimmer. The schematic refers to Figure 3. When the input signal of DIM pin is a 0-10V DC dimming voltage, the AL8116 will transfer the DC potential to a PWM signal and output at its OUT pin. The frequency of output PWM on AL8116 OUT pin is around 1.5kHz. Across an opto-coupler, the 1.5kHz PWM signal transfers to primary side, and is tied on to the AL1666A PWM pin. In this system application condition, the AL1666A operates in PWM-to-DC dimming mode.



### **Operation Parameters Design**

Setting the Current Sense Resistor Rcs

The current sense resistance can be calculated as following:

$$R_{CS} = \frac{N_{PS} \cdot V_{REF}}{2 \cdot I_{O\_MEAN}}$$

Where IO\_MEAN is the mean output current; RCs is current sense resister which is shown as Figure 1;

VREF is internal reference voltage that is equal to 0.4V; NPs is the turns ratio of Flyback transformer (NPs = 1 for Buck-boost).

#### Setting Transformer Selection (T1)

NPs is limited by the electrical stress of the switch MOSFET, can be calculated by below formula.

$$N_{PS} \leq \frac{V_{MOS\_(BR)DS} \cdot 90\% - \sqrt{2} \cdot V_{IN\_MAX} - \Delta V_S}{V_O + V_{D\_F}}$$

Where  $V_{MOS\_(BR)DS}$  is the breakdown voltage of the switch MOSFET.  $V_{IN\_MAX}$  is the max rated input voltage.  $\Delta V_S$  is the overshoot voltage clamped by RCD snobbier during OFF time. Vo is the output voltage.  $V_{D\_F}$  is the forward voltage of secondary diode. NPs is the turns ratio of Flyback transformer (NPs = 1 for Buck-boost);

For boundary conduction mode and constant on time method, the peak current of primary inductance can be calculated as below.

$$I_{P} = \frac{2 \cdot \pi \cdot I_{O\_MEAN}}{N_{PS} \cdot \int_{0}^{\pi} \sin(\theta) \cdot \frac{\sqrt{2} \cdot V_{IN\_RMS} \cdot \sin(\theta)}{\sqrt{2} \cdot V_{IN\_RMS} \cdot \sin(\theta) + N_{PS} \cdot Vo} d\theta}$$

Where V<sub>IN\_RMS</sub> is the rate input voltage; IP is the primary inductance current. NPs is the turns ratio of Flyback transformer (NPs = 1 for Buck-boost); IO\_MEAN is the mean output current; Vo is the output voltage.

The switching frequency is not constant for AL1666A due to boundary conduction mode. To set the minimum switching frequency f<sub>MIN</sub> at the crest of the minimum AC input, primary inductance can be obtained by below formula.

$$L_{P} = \frac{\sqrt{2} \cdot V_{IN\_RMS} \cdot N_{PS} \cdot V_{O}}{I_{P} \cdot (\sqrt{2}V_{IN\_RMS} + N_{PS}V_{O}) \cdot f_{MIN}}$$

Where VIN\_RMS is the rate input voltage; IP is the primary inductance current. NPs is the turns ratio of Flyback transformer (NPs = 1 for Buck-boost);

IO\_MEAN is the mean output current; Vo is the output voltage; fMIN is the minimum switching frequency at the crest of the minimum AC input.

According to the Faraday's Law, the winding number of the inductance can be calculated by:

$$N_{P} = \frac{L_{P} \cdot I_{P}}{A_{e} \cdot B_{m}}$$
$$N_{S} = \frac{N_{P}}{N_{PS}}$$

Where,

 $A_{e}$  is the core effective area.  $B_{m} \mbox{ is the maximum magnetic flux density}.$ 



# **Ordering Information**



Part Number	Package Code	ckage Code Package Package		cking	Part Number Suffix
Part Number Packag	Fackage Coue	achage coue Fachage	Qty.	Carrier	
AL1666AS-13	S	SO-8 (Standard)	4000	13" Tape & Reel	-13

# **Marking Information**





# **Package Outline Dimensions**

Please see http://www.diodes.com/package-outlines.html for the latest version.

#### SO-8 (Standard)



# **Suggested Pad Layout**

Please see http://www.diodes.com/package-outlines.html for the latest version.



SO-8 (Standard)

Dimensions	Value (in mm)
С	1.27
Х	0.802
X1	4.612
Y	1.505
Y1	6.50

## **Mechanical Data**

- Moisture Sensitivity: Level 1 per JESD22-A113
- Terminals: Finish Matte Tin Plated Leads, Solderable per M2003 JESD22-B102 (3)
- Weight: 0.076 grams (Approximate)



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