

#### THE AL17150-10B IS <u>NOT</u> RECOMMENDED FOR NEW DESIGNS. PLEASE USE THE <u>AP3917D</u>.



AL17150-10B

## HIGH-VOLTAGE STEP-DOWN SWITCHER UP TO 300mA OUTPUT CURRENT

## Description

The AL17150-10B is a universal high-voltage input step-down regulator product family, which provides accurate Constant Voltage (CV) and outstanding dynamic performance without requiring an optocoupler over line and load regulation. Typical applications are offline low-power applications including connected LED lighting power supply for micro-controllers and other IoT applications.

The AL17150-10B integrates a 500V/1A MOSFET that can make it use fewer external components and create a low Bill Of Material (BOM) cost solution. The AL17150-10B can provide up to 300mA output current and lower than 50mW standby power, which is very suitable for IoT connected lighting devices.

The AL17150-10B achieves excellent regulation and high power efficiency. The characteristics of max peak current and driving frequency vary as the load change, which can get excellent efficiency performance at light load and improve the overall average efficiency.

The AL17150-10B has rich protection features to enhance the system safety and reliability. It has Overtemperature Protection, V<sub>CC</sub> Undervoltage Lock function, Output Short Protection, Overload Protection and Open-Loop Protection.

The AL17150-10B is available in SO-7 package.

### **Features**

- Universal 85 to 265 VAC Input Range
- Internal MOSFET: 500V/1A
- Tight VFB tolerance ±4%
- Maximum 300mA Rated Output Current
- No Load Power Consumption: < 50mW with External Bias</li>
- Frequency Modulation to Suppress EMI
- Undervoltage Lockout (UVLO)
- Output Short Protection
- Overload Protection
- Thermal Shutdown (TSD)
- Fewer Components
- Low Audible Noise Solution
- SO-7 Package
- Totally Lead-Free & Fully RoHS Compliant (Notes 1 & 2)
- Halogen and Antimony Free. "Green" Device (Note 3)
- For automotive applications requiring specific change control (i.e. parts qualified to AEC-Q100/101/104/200, PPAP capable, and manufactured in IATF 16949 certified facilities), please <u>contact us</u> or your local Diodes representative.

https://www.diodes.com/quality/product-definitions/

Notes: 1. No purposely added lead. Fully EU Directive 2002/95/EC (RoHS), 2011/65/EU (RoHS 2) & 2015/863/EU (RoHS 3) compliant.

- 2. See https://www.diodes.com/quality/lead-free/ for more information about Diodes Incorporated's definitions of Halogen- and Antimony-free, "Green" and Lead-free.
- 3. Halogen- and Antimony-free "Green" products are defined as those which contain <900ppm bromine, <900ppm chlorine (<1500ppm total Br + Cl) and <1000ppm antimony compounds.

## Pin Assignments



## Applications

- IoT connected lighting applications
- Home appliance applications
- Industrial controls
- Standby and auxiliaries



## **Typical Applications Circuit**



## **Pin Descriptions**

Pin Number	Name	Function				
1, 2	N/C	Not Connected.				
3, 4	S	Internal Power MOSFET Source, Ground Reference for VCC and FB Pins.				
5	VCC	Connection Point of External Bypass Capacitor for Internally Generated Control Circuit Power Supply.				
6	FB	Regulator Feedback.				
7	Drain	Internal Power MOSFET Drain. High-Voltage Current Source Input.				
μ	_					

# Functional Block Diagram





## Absolute Maximum Ratings (Note 4)

Symbol	Parameter	Rating	Unit
V <sub>DSS</sub>	Voltage of Drain to S pin	-0.7 to 500	V
VFB	Voltage of FB to S Pin	-0.7 to 6.5	V
Vcc	Operating VCC Voltage	8.9	V
PD	Continuous Power Dissipation ( $T_A = +25^{\circ}C$ )	1	W
TJ	Operating Junction Temperature	+150	°C
Tstg	Storage Temperature	-65 to +150	°C
TLEAD	Lead Temperature (Soldering, 10s)	+300	°C
θ <sub>JA</sub>	Thermal Resistance (Junction to Ambient)	139	°C/W
θ <sub>JC</sub>	Thermal Resistance (Junction to Case)	21	°C/W
505	ESD (Human Body Model)	4000	V
ESD	ESD (Charge Device Model)	1000	V

Note: 4. Stresses greater than those listed under Absolute Maximum Ratings can cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions is not implied. Exposure to Absolute Maximum Ratings for extended periods can affect device reliability.

# **Recommended Operating Conditions**

Symbol	Parameter	Min	Мах	Unit
Vcc	Supply Voltage	8.2	8.8	V
Та	Ambient Temperature	-40	+125	°C
Ιουτ	Output Current with 3.3V/5V Output Voltage		300	mA



## Electrical Characteristics (V<sub>CC</sub> = 8.8V, T<sub>A</sub>=+25°C, unless otherwise specified.)

Symbol	Parameter	Condition	Min	Тур	Max	Unit
HV Startup Curr	ent Source				1	
Іну	HV Supply Current	Vcc = 7V; Vdrain = 100V	1.2	3.5	—	mA
ILEAK	Leakage Current of Drain	Vcc = 8.8V; Vdrain = 400V	_	10	12	μA
Vcc Voltage Mar	nagement					
Vcc_off	VCC Supply OFF Threshold Voltage	_	8.1	8.5	8.8	V
V <sub>CC_ON</sub>	VCC Supply ON Threshold Voltage	—	7.8	8.2	8.6	V
	VCC Supply ON and OFF Hysteresis	_	-	280	_	mV
Vcc_uvlo	Minimum Operating Voltage	—		6.5	_	V
Vcc_restart	Restart Voltage	_	_	4.5	_	V
lcc	Operating Current	Vcc = 7.5V, fs = 40kHz, D = 40%		350	-	μA
lcc_qc	Quiescent Current with No Switching			110	200	μA
ICC_LATCH	Latch Off Current	-	—	26	-	μA
Internal MOSFE	r					
V <sub>DS</sub>	Breakdown Voltage (Note 5)	-	500	I	—	V
R <sub>DS(ON)</sub>	ON Resistance			_	12	Ω
Internal Current	Sense					
Ірк_мах	Peak Current		413	500	600	mA
t <sub>LEB</sub>	Leading Edge Blanking Time		_	250	400	ns
I <sub>SCP</sub>	SCP Point Current	-		800	_	mA
Feedback Input	(FB Pin)					
<b>t</b> MINOFF	Minimum Off Time		10.5	15.5	18.5	μS
Vfb	MOSFET Feedback Switch-On Threshold		2.4	2.5	2.6	V
Vfb_olp	OLP Feedback Trigger Threshold		1.56	1.7	1.84	V
tolp	OLP Delay Time	fs = 37kHz	_	170	_	ms
Vold	Open-Loop Detection	Y	_	60	_	mV
told	OLD Active Time	fs = 15kHz	_	4.3	—	ms
Thermal Shutdo	wn					
Tsd	Thermal Shutdown Threshold	_	+135	+150	+165	°C

Note: 5. The drain-source voltage is 80% of VDSS in the aging condition.



## Typical Characteristics (Note 6)



Feedback Threshold Voltage vs. Ambient Temperature

Minimum Operating Voltage vs. Ambient Temperature

Note: 6. These electrical characteristics are tested under DC condition. The ambient temperature is equal to the junction temperature of the device.



## **Function Description**

#### **Overall Introduction**

The AL17150-10B is a universal AC input step down regulator. Max peak current limitation and driving frequency vary as the load change can get excellent efficiency performance at light load and improve the overall efficiency of system. Working with a single winding inductor and integrating 500V/1A MOSFET internal can make it use fewer external components and create a low BOM cost solution. Figure 1 shows a typical application example of a buck topology power supply.



Figure 1. Typical Application Circuit

#### **Converter Operation**

#### Startup and Undervoltage Lockout

The IC control voltage Vcc is charged by internal high-voltage regulator. When the Vcc voltage is charged to 8.5V, IC startups and the internal high voltage regulator is turned off; when the Vcc voltage drops below 8.2V, the internal high voltage regulator turns on again to charge the external VCC capacitor.

When fault conditions happen, such as some protections like overload faults, short-circuit faults, overtemperature faults, and open-loop faults, the AL17150-10B stops switching. Afterwards an internal current source IBP\_LATCH discharges the external BP capacitor. The internal high-voltage regulator will not turn on again until the voltage on BP capacitor drops below VBP\_RESTART (4.5V). The restart time interval is proportional to the capacitance of external BP capacitor—the larger capacitance of the external BP capacitor, the longer restart time.

The restart time after a fault is about

$$t_{RESTART} = C_{VCC} \times \left( \frac{V_{CC,FAULT} - V_{CC,RESTART}}{I_{CC_{LATCH}}} + \frac{V_{CC,OFF} - V_{CC,RESTART}}{I_{HV}} \right)$$
(1)

Where:

V<sub>CC\_FAULT</sub> is actual voltage value of VCC pin at the time of fault, which is between V<sub>CC\_ON</sub> and V<sub>CC\_OFF</sub>.

#### Figure 2 shows the typical waveform of Vcc.





#### Auxiliary VCC Supply

If the output voltage is higher than the voltage of V<sub>CC\_ON</sub>, an auxiliary V<sub>CC</sub> supply can be implemented to reduce overall power consumption by connecting a resistor (R4) between C2 and C3. A standby power of less than 50mW can be achieved especially in a no-load condition.



Figure 3 shows the low standby power circuit with the auxiliary Vcc supply.



The value of R4 can be determined by the following equation:

$$R4 = \frac{V_O - V_{CC_ON}}{I_{CC_QC}} \dots$$

#### **Constant Voltage Operation**

The AL17150-10B is a step-down regulator with 500V/1A MOSFET internal. It can be used in buck circuit as shown in the *Typical Application Circuit*.

In the course of running IC, when the voltage of FB pin is below the reference voltage (2.5V), the internal integrated MOSFET turns ON. The peak current limit and the initial inductance current value altogether with the input voltage determine the ON period time. When the current reaches peak current limit, the internal integrated MOSFET turns OFF. The inductor current charges the sampling capacitor (C5) and the output capacitor (C6) via the freewheeling diode D4 and D3 respectively. The sampling capacitor voltage is the mapping of the output voltage. The output voltage can be controlled by sampling the voltage of feedback pin which is derived from the voltage of sampling capacitor. In the OFF stage of internal MOSFET, when the inductor current drops below the output current, the sampling capacitor voltage begins to decrease. When the voltage of feedback pin falls below the reference voltage (2.5V), a new switching cycle begins.

Figure 4 shows the detailed operation timing diagrams under Discontinuous-Conduction Mode (DCM) and Continuous-Conduction Mode (CCM).



Figure 4. Operation Timing of AL17150-10B



Generally, the output voltage can be described as the following equation:

 $V_0 = 2.5 \times (R_1 + R_2)/R_2$  (3)

#### **Frequency and Peak Current**

To maintain high efficiency under different load condition, the AL17150-10B adjusts the switching frequency automatically. The switching frequency can be calculated with Equation 4 for DCM mode operation and Equation 5 for CCM mode operation.

$$f_{s} = \frac{2(V_{IN} - V_{O})}{L \cdot l_{PK}^{2}} \cdot \frac{l_{O}V_{O}}{V_{IN}}.$$
(4)
$$f_{s} = \frac{(V_{IN} - V_{O})}{2L \cdot (l_{PK} - l_{O})} \cdot \frac{V_{O}}{V_{IN}}.$$
(5)

In the meantime, the peak current of the inductor (IPK) is determined by the following equation:

$$I_{PK} = 500mA - (4mA/\mu s) \times (t_{OFF} - 15.5\mu s) \dots (6)$$

In the Equation 6, toFF is internal MOSFET OFF time of the IC, and 500mA is peak current limit and 15.5µs is the minimum toFF value.

As the load decreases, the switching frequency decreases and the MOSFET OFF time toFF increases, leading to the decrease of peak current. In no load condition, in which only a dummy load is retained, the frequency and the peak current are both minimized. This helps to reduce the no load power consumption.

#### Startup Control

The AL17150-10B implements a minimum OFF time control. In normal condition, the minimum OFF time limit is 15.5µs.

In the startup process, the output voltage is not established and more demagnetizing time is needed. Therefore, the soft start technique is adopted. During the startup process, the minimum MOSFET OFF time varies with three stages, and it gradually drops from 60µs to 30µs, and then to 15.5µs. Each stage contains 128 switching cycles and the startup process will end if the desired output voltage is reached.

#### **EA Compensation**

To improve load regulation and load transient performance, the AL17150-10B is designed with an Error Amplifier (EA) compensation function.

The compensation is related to the load condition. With an increasing load, the compensation value increases and the reference voltage of the internal feedback comparator is slightly pulled down. A faster change in the load will lead to a greater compensation step. The output voltage will be regulated back to the desired voltage. This compensation will precisely maintain the output voltage.

#### Leading-Edge Blanking

A narrow spike on the leading edge of the current waveform can usually be observed when the power MOSFET is turned on. A 250ns leadingedge blank is built-in to prevent the false-triggering caused by the turn-on spike. During this period, the current limit comparator is disabled and the gate driver cannot be switched off.

#### Protection

#### Short-Circuit Protection (SCP)

The AL17150-10B will shut down when the peak current exceeds the short-circuit protection threshold (800mA). The AL17150-10B will resume operation when the fault is removed.

#### **Overload Protection (OLP)**

With the increase of load, the peak current and the switching frequency increase. When the peak current reaches the maximum limitation, and the OFF time is the minimum OFF time, the output voltage drops if the load continues to increase. Similarly, the FB voltage decreases as the output voltage drops. When FB voltage drops below OLP threshold  $V_{FB_OLP}$  (1.7V), the internal timer of overload starts to count. Once the overload duration lasts more than the OLP delay time t<sub>OLP</sub> (170ms), the OLP occurs.

The time delay setting of OLP should avoid triggering OLP when the system starts up or enters a load transition phase. Therefore it requires that the system startup time must be less than  $t_{OLP}$ . The 170ms time delay of  $t_{OLP}$  is calculated under the condition of 36kHz operating frequency. The different operating frequency corresponds to different time delay, the time delay calculation under different operating frequency (fs) as follows:

 $t_{DELAY} = 170ms \times \frac{36kHz}{r}$ fs

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When the V<sub>FB</sub> drops below 60mV, the AL17150-10B will stop working and begin a re-start cycle. The open-loop detection is blanked for 64 switching cycles during startup stage.

#### Thermal Shutdown (TSD)

The AL17150-10B integrates an internal thermal shutdown protection function. If the IC junction temperature rises above  $T_{JSTOP}$  (typical value: +150°C), the Thermal Shutdown (TSD) protection is triggered and the internal MOSFET stops switching. To recover the switching of internal MOSFET, the IC junction temperature has to fall by a hysteresis of +30°C below the  $T_{JSTOP}$ . During TSD protection,  $V_{CC}$  drops to  $V_{CC_{RESTART}}$  (typical value 4.5V), and then the internal high-voltage regulator recharges  $V_{CC}$ .

#### Application and Implementation

The AL17150-10B is a universal high-voltage step-down regulator. Figure 1 shows a typical application for reference. The application can be used in a wide variety of home appliances and industrial control devices, or any other application where mains isolation is not required.

#### Input Stage

The input stage consists of RF1, D1, D2, C1, C2 and L1, Resistor RF1 is a fusible resistor. RF1 limits the inrush current, and also provides protection in case any component failure causes a short circuit. Value for its resistance is generally selected from  $4.7\Omega$  to  $15\Omega$ . A half-wave rectifier is implemented with the diode D1. It is a general-purpose 1A/1000V diode. D<sub>2</sub> is added for improving common-mode conducted EMI noise performance and can be removed if not needed. Components C1, L1, C2 form a Pi EMI filter; Capacitors C1 and C2 also act as storage capacitors for the high-voltage input DC voltage.

When using the half-wave rectifier, set the input capacitor 3µF/W for the universal input condition. When using the full-wave rectifier, choose a smaller capacitor. To avoid thermal shutdown, capacitance selection must avoid the minimum DC voltage below 70V. And if passing surge test is needed for the converter, adjusting input capacitance can help to meet different surge test requirements.

#### Vcc Capacitor

The Vcc capacitor (C3) acts as the storage capacitor for the IC internal power supply. A typical selection is a 2.2µF/10V SMD ceramic capacitor.

#### Inductor

In buck converter, the inductor peak to peak current ripple can be obtained with Equation 8 for DCM mode operation and with Equation 9 for CCM mode operation.

$$\Delta I_L = I_{PK} \tag{8}$$

$$\Delta I_L = 2 \times (I_{PK} - I_{OUT})$$
(9)

The internal MOSFET turn-on time (ton) can be given by Equation 10 and it is determine by the peak current limit and the inductor.

$$t_{ON} = \frac{L \cdot \Delta I_L}{V_{IN} - V_O}$$
(10)

To guarantee normal operation,  $t_{\text{ON}}$  must be bigger than  $t_{\text{LEB}}$  with margin.

The Buck converter reaches maximum power when the off-time equals the minimum off time (tminoff). Thus the maximum output power can be calculated with Equation 11 for DCM mode operation and with Equation 12 for CCM mode operation.

$$P_{OMAX} = \frac{1}{2}L \cdot I_{PK}^2 \cdot \frac{1}{t_{ON} + t_{MINOFF}} \approx \frac{1}{2}L \cdot I_{PK}^2 \cdot \frac{1}{t_{MINOFF}}.$$
(11)
$$P_{OMAX} = V_O(I_{PK} - \frac{V_O t_{MINOFF}}{2L}).$$
(12)

Since the on-time is generally far smaller than the off-time, the approximation in Equation 8 can be reasonable for estimation.

To design an inductor, the desired maximum output power is given according to the output specification. The desired peak current is also estimated, no more than 500mA. Since  $t_{MINOFF}$  is 15.5µs, a minimum inductance can be calculated with Equation 8. The inductance should be checked with the above equations, and it should be adjusted to ensure that the on-time limitation is satisfied and the desired peak current under full load is met. Some inductance margin is also needed for tolerance.

With the inductance and its peak current value, a standard off-the-shelf inductor can be used to reduce cost.



#### Freewheeling Diode

The maximum reverse voltage that the diode would experience during normal operation is given by the following equation.

 $V_{D-MAX} = \sqrt{2} \times V_{INAC-MAX}.$ (13)

For a universal AC input application, the 265VAC, thus VD-MAX value is 375V. Considering a margin of 20%, a 600V diode is a general selection.

A fast recovery diode is required for the buck application. And the reverse-recovery time should be kept less than 100ns.

#### **Output Capacitor**

The output capacitor maintains the DC output voltage, and the value impacts the output ripple. The output voltage ripple can be estimated with Equation 14 for DCM mode operation and Equation 15 for CCM mode operation.

$$V_{OUT\_RIPPLE} = \frac{I_{OUT}}{f_S C_{OUT}} \cdot \left(\frac{I_{PK} - I_{OUT}}{I_{PK}}\right) + I_{PK} \cdot R_{ESR}.$$

$$(14)$$

$$V_{OUT\_RIPPLE} = \frac{\Delta I_L}{f_S C_{OUT}} + \Delta I_L \cdot R_{ESR}.$$

$$(15)$$

Where fs is the switching frequency, and R<sub>ESR</sub> is ESR of output capacitor. For a typical application, the capacitor value can ranges from 47µF to hundreds of µF. If the total ripple is higher than the requirement, increasing the capacitance and reducing the ESR can be helpful.

#### Dummy Load

The output requires a dummy load (R3) to maintain the load regulation under no-load condition. This can ensure sufficient inductor energy to charge the sample-and-hold capacitor to detect the output voltage. Most applications can use a 3mA dummy load, and the dummy load can be adjusted according to the regulation. Increasing the dummy load adversely affects the efficiency and no-load consumption.

#### Feedback Path

R1 and R2 form a resistor divider that determines the output voltage. The values of R1 and R2 should be set to maintain the FB voltage at 2.5V. The typical value for R2 is between  $5k\Omega$  to  $10k\Omega$  and precision of R1 and R2 must be 1%.

$$V_{OUT} = V_{FB} \cdot \frac{R_1 + R_2}{R_2} + V_{D3} - V_{D2} \approx V_{FB} \cdot \frac{R_1 + R_2}{R_2}.$$
(16)

For low output voltage application, the difference caused by D3 and D4 cannot be neglected and R1 should be set larger to compensate the difference. Since the diode forward voltage is positively related with the current flows through it and the current through D3 is much higher than D4, V<sub>D3</sub> is higher than V<sub>D4</sub>.

The feedback capacitor provides a sample and hold function and the capacitance selection should follow the Equation 17 as below.

$$\frac{V_{OUT}}{2(R_1+R_2)} \cdot \frac{C_6}{I_{OUT}} < C_5 < \frac{V_{OUT}}{(R_1+R_2)} \cdot \frac{C_6}{I_{OUT}}.$$
(17)

The capacitor C5 is discharged with a time constant that is  $\tau_{FB} = C_5 \cdot (R_1 + R_2)$  and  $\tau_{out} = C_6 \cdot V_{OUT}/I_{OUT}$  can be regarded as the load time constant. If  $\tau_{FB}$  is larger than  $\tau_{out}$ , voltage on C5 could be larger than Vour when sampling, leading to wrong sampling of Vour and wrong regulation. And if  $\tau_{FB}$  is too small, voltage on FB pin would drop to 1.7V before the next MOSFET OFF time come and thus mis-trigger Overload Protection (OLP). Therefore, an appropriate value of C5 is important.

#### Layout Guidelines

The PCB layout is important to achieve reliable operation, good EMI, and thermal performance. Follow these guidelines to optimize performance.

- Minimize the loop area formed by the input capacitor, IC part, freewheeling diode, inductor and output capacitor.
- The copper area of the FB signal should be minimized to reduce coupling to feedback path.
- A several-hundred pF capacitor should be added between the FB and S pins, and be placed as close as to the FB pin as possible.
- Place the power inductor far away from the input filter.
- · Connect the exposed pad with the Drain pin to a large copper area to improve thermal performance.



## **Ordering Information**





## Package Outline Dimensions (All dimensions in mm(inch).)

Please see http://www.diodes.com/package-outlines.html for the latest version.

#### Package Type: SO-7



### **Suggested Pad Layout**

Please see http://www.diodes.com/package-outlines.html for the latest version.



Dimensions	Z	G	X	Y	E	E1
	(mm)/(inch)	(mm)/(inch)	(mm)/(inch)	(mm)/(inch)	(mm)/(inch)	(mm)/(inch)
Value	6.900/0.272	3.900/0.154	0.650/0.026	1.500/0.059	1.270/0.050	2.540/0.100



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